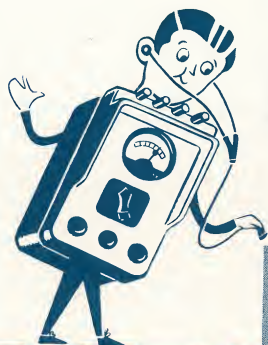


GETTING DOWN-TO-EARTH



MANUAL ON EARTH-RESISTANCE TESTING

FOR THE PRACTICAL MAN



JAMES G. BIDDLE CO.
PLYMOUTH MEETING, PENNSYLVANIA 19462

“Getting down to earth...”

**A Manual on
EARTH-RESISTANCE TESTING
for the practical man**

- Electrical grounding systems
- Earth resistivity

FIRST EDITION
MARCH 1966

Copyright, 1966

JAMES G. BIDDLE CO.
ELECTRICAL AND SCIENTIFIC INSTRUMENTS

PLYMOUTH MEETING, PA. 19462

FIFTY CENTS PER COPY

A DOWN-TO-EARTH SUBJECT . . . VITAL TO INDUSTRY AND SCIENCE

Nothing is quite so common or abundantly available throughout the world as the earth's soil. We're more apt to think of earth as something to be tilled for planting, or to be excavated for a building foundation. Yet, it also has an electrical property—conductivity (or low resistance)—that is being put to very practical use every day in industrial plants and utilities.

Broadly speaking, "earth resistance" is the resistance of soil to the passage of electric current. Actually, the earth is a relatively poor conductor of electricity compared to normal conductors like copper wire. But, if the area of a path for current is large enough, resistance can be quite low and the earth can be a good "conductor."

Measurement of earth resistance is made in two ways for two important fields of use:

1. Determining the effectiveness of "ground" grids and connections which are used with electrical systems to protect personnel and equipment.
2. Prospecting for good (low resistance) "ground" locations, or obtaining measured resistance values which can give specific information about what lies some distance below the earth's surface (such as depth to bed rock).

It is not the intent of this manual to go too deeply into the theory and mathematics of the subject. As covered in the references at the end, there are many excellent books and papers that cover these. Rather, the coverage herein is in simple language for easy understanding by the user in industry.

From years of experience in supplying instruments for the tests involved, James G. Biddle Co. can provide much practical advice to help you make specific tests and will be pleased to have a representative call on you to discuss your problem. For this free service, or copies of literature, simply use one of the postpaid cards included in the back of this manual.

JAMES G. BIDDLE CO.
Plymouth Meeting, Pa.



Photograph courtesy of Philadelphia Electric Co.

Earth-resistance test being made at a large power company substation.

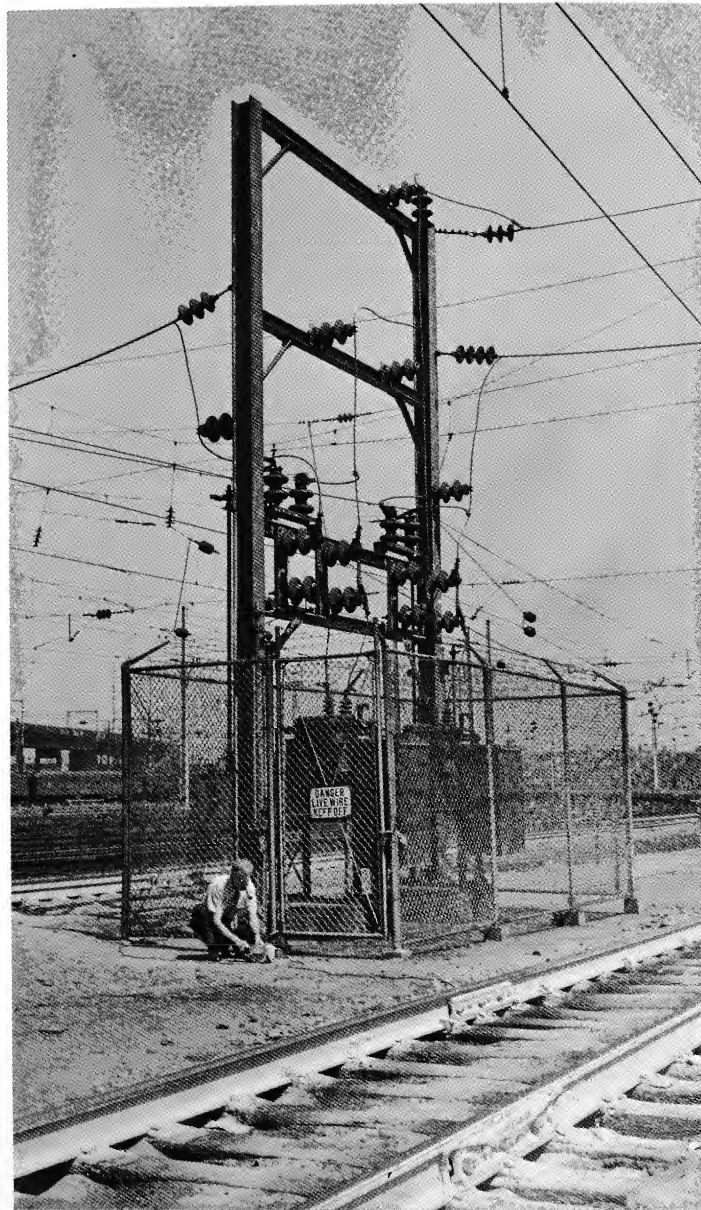
TABLE OF CONTENTS

	PAGE
INTRODUCTION	2
SECTION I—MEASURING EARTH RESISTANCE FOR ELECTRICAL GROUNDING SYSTEMS	7
THREE FACTORS THAT CAN CHANGE YOUR “MINIMUM” EARTH RESISTANCE	8
SOME BASIC DEFINITIONS	8
FACTORS INFLUENCING REQUIREMENTS FOR A GOOD GROUNDING SYSTEM	10
NATIONAL ELECTRICAL CODE MAXIMUM VALUES	12
NATURE OF AN EARTH ELECTRODE	13
Electrode Resistance	13
Electrode-Earth Contact Resistance	13
Resistance of Surrounding Earth	13
PRINCIPLES INVOLVED IN EARTH-RESISTANCE TESTING	14
BASIC TEST METHODS FOR EARTH RESISTANCE	18
Direct Method	18
Fall-of-Potential Method	19
EFFECTS OF DIFFERENT REFERENCE PROBE LOCATIONS	20
Minimum Distance for C_2	20
Simplified Fall-of-Potential Test	22
Some Rules of Thumb on Spacing P_2 and C_2	22
TABLE I—Guide to Approximate Location of Reference Probes	23
HOW TO IMPROVE EARTH RESISTANCE	24
Effect of Rod Size	24
Use of Multiple Rods	25
Treatment of the Soil	27
SECTION II—EARTH RESISTIVITY	29
HOW EARTH RESISTIVITY IS MEASURED	30
PRACTICAL EXAMPLE OF TEST METHOD	31
TYPE OF SOIL AFFECTS RESISTIVITY	32
TABLES II and III—Resistivities of Different Soils	32
RESISTIVITY DECREASES WITH MOISTURE AND DISSOLVED SALTS	33
TABLE IV—Effect of Moisture Content on Earth Resistivity	33
TABLE V—Effect of Salt Content on Earth Resistivity	34
EFFECT OF TEMPERATURE ON EARTH RESISTIVITY	34
TABLE VI—Effect of Temperature on Earth Resistivity	34
SEASONAL VARIATIONS IN EARTH RESISTIVITY	35
DETERMINING A GOOD ELECTRODE LOCATION	38
Alternate Method	39
NOMOGRAPH GUIDE TO SETTING ACCEPTABLE EARTH RESISTANCE	40
REFERENCES	42

LIST OF ILLUSTRATIONS

	PAGE
Fig. 1—A simplified grounding system in an industrial plant	7
Fig. 2—Example of an electrical circuit with too high an earth resistance	9
Fig. 3—Typical conditions to be considered in a plant grounding system	10
Fig. 4—Components of earth resistance in an earth electrode	13
Fig. 5—Principle of an earth-resistance test	17
Fig. 6—“Direct Method” or “Two-Terminal” earth-resistance test	18
Fig. 7—“Fall-of-Potential” or “Three-Terminal” earth-resistance test	19
Fig. 8—Effect of C_2 location on the earth-resistance curve	21
Fig. 9—Example of how C_2 location affects the earth-resistance curve	22
Fig. 10—Earth resistance decreases with depth of electrode in earth	24
Fig. 11—Diameter of a rod has little effect on its earth resistance	25
Fig. 12—Average results obtained from multiple-rod earth electrodes	26
Fig. 13—Comparative resistance of multiple-rod earth electrodes	26
Fig. 14—Trench method of soil treatment	27
Fig. 15—Chemical treatment of soil lessens seasonal variation of electrode’s earth-resistance	28
Fig. 16—“Four-Terminal” method of measuring earth resistivity	30
Fig. 17—Earth-resistivity survey of pipeline shows where corrosion is most likely to occur	31
Fig. 18—Deeper earth electrodes lower the resistance. These graphs show the relation between character of soil and resistance of driven electrode at increased depths	33
Fig. 19—Seasonal variation of earth resistance with an electrode of $\frac{3}{4}$ -inch pipe in rather stony clay soil	37
Fig. 20—Method of prospecting for best earth electrode location	38
Fig. 21—Nomograph relating the basic factors affecting earth resistance	41

NOTE: As used in this manual, “MEGGER” is a trademark—registered in the U.S. Patent Office, like “Hotpoint” or “Palmolive.” It applies to other similar instruments, such as Megger Electrical Insulation Testers, made and sold in the U.S.A. exclusively by James G. Biddle Co.



Photograph courtesy of Pennsylvania Railroad Co.

Checking the earth-resistance of a grounding system at an electric railroad substation.

SECTION I

Measuring Earth Resistance For Electrical Grounding Systems

The simplest and somewhat misleading idea of a good "ground" for an electrical system is a section of iron pipe driven into the earth with a wire conductor connected from the pipe to the electrical circuit (Fig. 1). This may, or may *not*, be a suitable low resistance path for electric current to protect personnel and equipment.

A *practical* earth electrode that provides a low ground resistance is not always easy to obtain. But from experience gained by others you can learn how to set up a reliable system and how to check the resistance value with reasonable accuracy. As you will see, earth resistivity (Part II) has an important bearing on electrode resistance, as does the depth, size, and shape of the electrode.

The principles and methods of *earth-resistance testing* covered in this section apply to lightning arrester installations as well as to other systems that require low-resistance ground connections. Such tests are made in power-generating stations, electrical-distribution systems, industrial plants, and telecommunication systems.

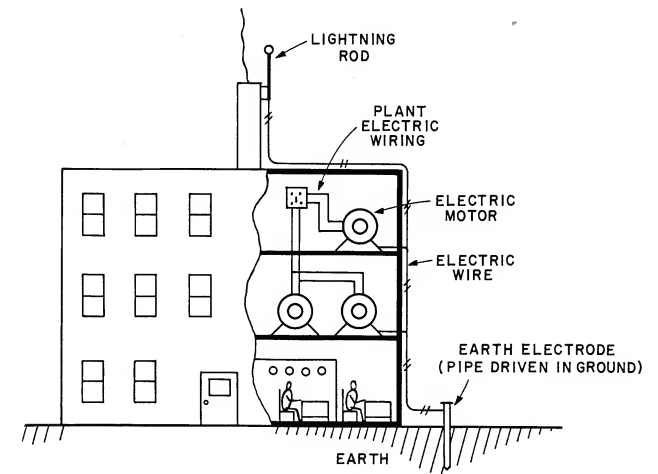


Fig. 1—A simplified grounding system in an industrial plant.

THREE FACTORS THAT CAN CHANGE YOUR "MINIMUM" EARTH RESISTANCE

We will discuss later what value of earth resistance is considered low enough. You'll see that there's no general rule usable for all cases. First, however, consider three factors that can *change* the earth electrode requirements from year to year:

1. A plant or other electrical facility can expand in size. Also, new plants continue to be built larger and larger. Such changes create different needs in the earth electrode. What was formerly a suitably low earth resistance can become an obsolete "standard."
2. As more non-metallic pipes and conduits are installed underground, such installations become less and less dependable as effective, low-resistance ground connections.
3. In many locations, the water table is gradually falling. In a year or so, earth electrode systems that formerly were effective may end up in dry earth of high resistance.

These factors emphasize the importance of a continuous, periodic program of earth-resistance testing. It is not enough to check the earth resistance only at the time of installation.

SOME BASIC DEFINITIONS

First, let's define our terms. As early as 1918*, the terms *ground*, *permanent ground*, and *ground connections* were defined to mean "electrical connections intentionally made between electrical bodies (or conducting bodies in close proximity to electrical circuits) and metallic bodies in the earth—such as rods, water pipes, plates, or driven pipes."

The *metallic body* in the earth is often referred to as an *electrode* even though it may be a water-pipe

* Reference 19

system, buried strips or plates, or wires. Such combinations of metallic bodies are called a *grid*. The *earth resistance* we're concerned with is the resistance to current from the *electrode* into the surrounding earth.

To appreciate why earth resistance must be low, you need only use Ohm's Law: $E = R \times I$ —where E is volts; R , the resistance in ohms; and I , the current in amperes. Assume that you have a 4,000-volt supply (2,300 volts to "ground") with a resistance of 13 ohms (see Fig. 2). Now, assume that an exposed wire in this system touches a motor frame that is connected to a grounding system which has a 10-ohm resistance to earth.

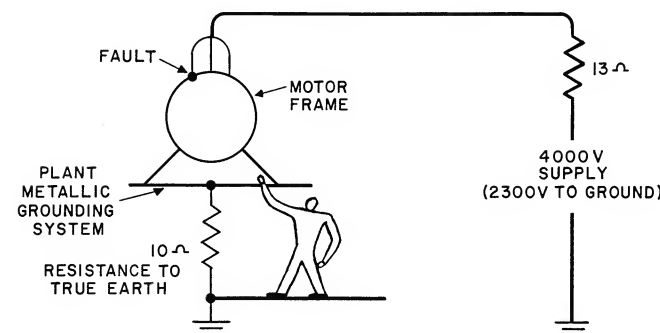


Fig. 2—Example of an electrical circuit with too high an earth resistance.

By Ohm's Law, there will be a current of 100 amperes** through the *fault* (from the motor frame to the earth). If you happen to touch the motor frame and are grounded solidly to earth, (say, by standing in a puddle) you could be subjected to 1,000 volts (10 ohms times 100 amperes).

As you'll note from Point 2, page 11, this may be much more than enough to kill you instantly. If, however, the earth resistance is less than one ohm, the "shock" you'd get would be under 100 volts (1×100) and you'd probably live to correct the fault.

Equipment can also be damaged similarly by over-voltages caused by high-resistance grounding systems.

$$** I = \frac{E}{R} = \frac{2,300}{10 + 13} = 100 \text{ amp.}$$

FACTORS INFLUENCING REQUIREMENTS FOR A GOOD GROUNDING SYSTEM

In an industrial plant or other facility that requires a grounding system, one or more of the following must be carefully considered (See Fig. 3):

1. *Limiting to definite values the voltage to earth of the entire electrical system.* Use of a suitable grounding system can do this by maintaining some point in the circuit at earth potential. Such a grounding system provides these advantages:
 - a. Limits voltage to which the system-to-ground insulation is subjected, thereby more definitely fixing the insulation rating.
 - b. Limits the system-to-ground or system-to-frame voltage to values safe for personnel.
 - c. Provides a relatively stable system with a minimum of transient overvoltages.
 - d. Permits any system fault to ground to be quickly isolated.

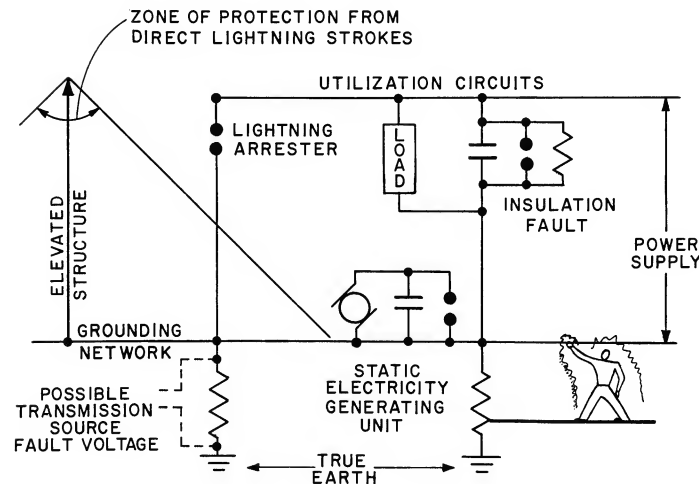


Fig. 3—Typical conditions to be considered in a plant grounding system.

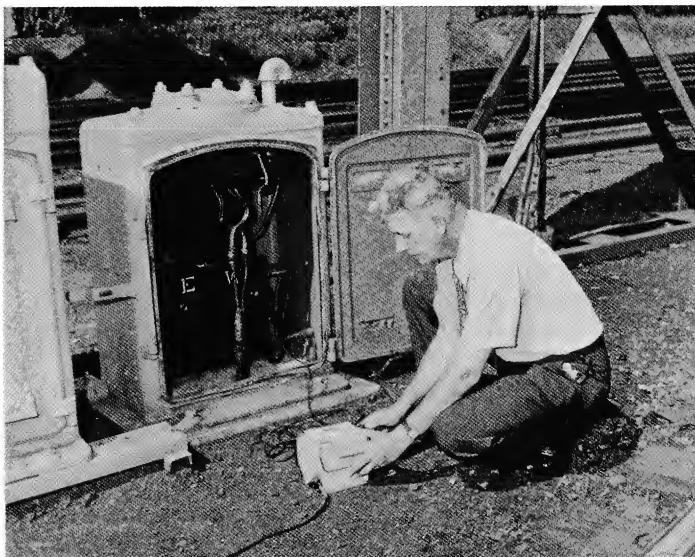
2. *Proper grounding of metallic enclosures and supporting structures* that are part of the electrical system and may be contacted by personnel. Also, to be included are portable electrically-operated devices. Consider that only a small amount of electric current—as little as 0.1 ampere for one second—can be fatal! An even smaller amount can cause you to lose muscular control. These low currents can occur in your body at voltages as low as 100 volts, if your skin is moist.
3. *Protection against static electricity from friction.* Along with this are the attendant hazards of shock, fire and explosion. Moving objects that may be inherent insulators—such as paper, textiles, conveyor belts or power belts and rubberized fabrics—can develop surprisingly high charges unless properly grounded.
4. *Protection against direct lightning strokes.* Elevated structures, such as stacks, the building proper, water tanks, etc.—may require lightning rods connected into the grounding system.
5. *Protection against induced lightning voltages.* This is particularly a factor if aerial power distribution and communications circuits are involved. Lightning arresters may be required in strategic locations throughout the plant.
6. *Providing good grounds for electric process control and communication circuits.* With the increased use of industrial control instruments, computers, and communications equipment, accessibility of low-resistance ground connections in many plant locations—in office and production areas—must be considered.

NATIONAL ELECTRICAL CODE MAXIMUM VALUES

The National Electrical Code states “. . . made electrodes shall, where practical, have a resistance to ground not to exceed 25 ohms. Where the resistance is not as low as 25 ohms, two or more electrodes connected in parallel shall be used. It is always recommended that single-electrode grounds be *tested when installed, and periodically afterward.*”

We italicized the last phrase because of its importance. Resistance to earth can vary with changes in climate and temperature. Such changes can be considerable. An earth electrode that was good (low-resistance) when installed may not stay that way; to be sure, you must check it periodically.

We cannot tell you what your maximum earth resistance should be. For specific systems in definite locations, specifications are often set. Some call for 5 ohms maximum; others accept no more than 3 ohms. In certain cases, resistances as low as a small fraction of an ohm are required.



Photograph courtesy of Pennsylvania Railroad Co.

Megger “earth-tester” being used to check grounding system at railroad signal tower.

NATURE OF AN EARTH ELECTRODE

Resistance to current through an earth electrode actually has three components (Fig. 4):

1. Resistance of the electrode itself and connections to it.
2. Contact resistance between the electrode and the soil adjacent to it.
3. Resistance of the surrounding earth.

Electrode Resistance: Rods, pipes, masses of metal, structures, and other devices are commonly used for earth connections. These are usually of sufficient size or cross-section that their resistance is a negligible part of the total resistance.

Electrode-Earth Contact Resistance: This is much less than you might think. If the electrode is free from paint or grease, and the earth is packed firmly, the Bureau of Standards has shown that contact resistance is negligible. Rust on an iron electrode has little or no effect; the iron oxide is readily soaked with water and has less resistance than most soils. But if an iron pipe has rusted through, the part below the break is not effective as a part of the earth electrode.

Resistance of Surrounding Earth: An electrode driven into earth of uniform resistivity radiates current in all directions. Think of the electrode as being surrounded by *shells of earth*, all of equal thickness (see Fig. 4).

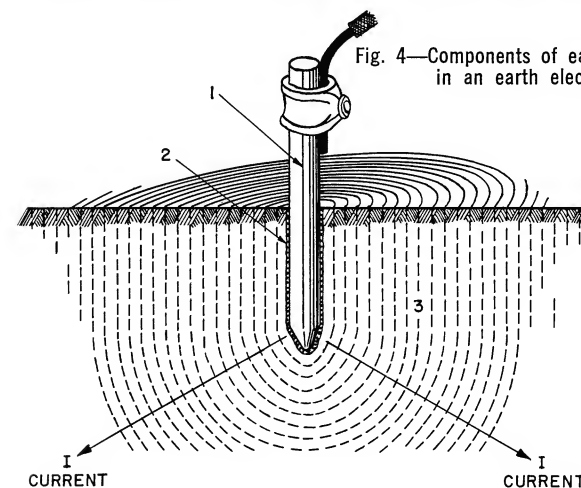


Fig. 4—Components of earth resistance in an earth electrode.

The earth shell nearest the electrode naturally has the smallest surface area and so offers the greatest resistance. The next earth shell is somewhat larger in area and offers less resistance. And so on out. Finally, a distance from the electrode will be reached where inclusion of additional earth shells does not add significantly to the resistance of the earth surrounding the electrode.

*Generally, the resistance of the surrounding earth will be the largest of the three components making up the resistance of a ground connection. The several factors that can affect this value are discussed in Section II on Earth Resistivity. From Section II, you'll see that earth resistivity depends on the soil material, the moisture content, and the temperature. It is far from a constant, predictable value—ranging generally from 500 to 50,000 ohm-cm.**

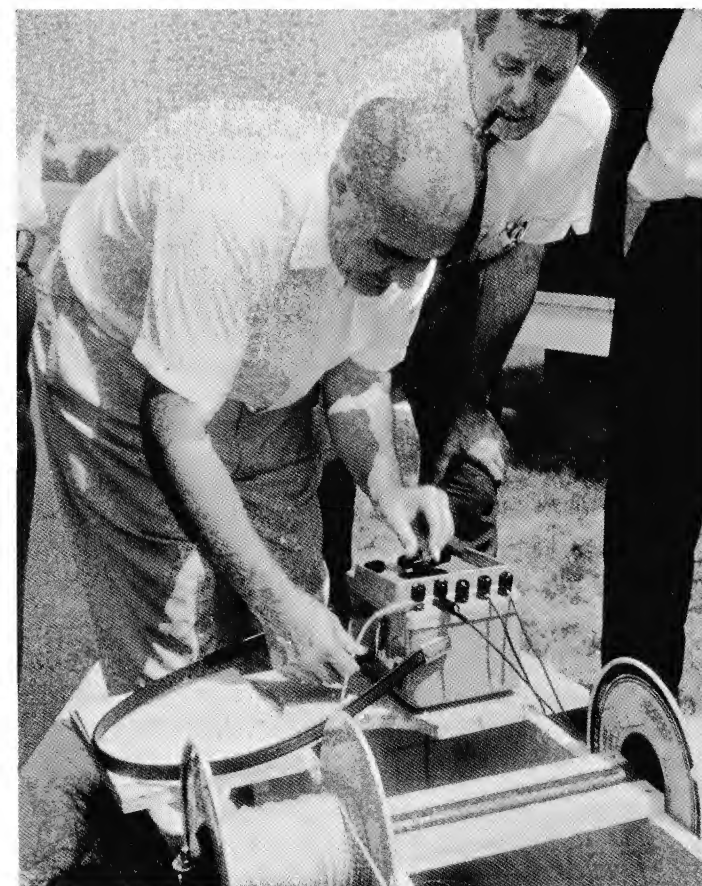
PRINCIPLES INVOLVED IN EARTH-RESISTANCE TESTING

The resistance to earth of any system of electrodes *theoretically* can be calculated from formulas based upon the general resistance formula:

$$R = \rho \frac{L}{A}$$

where ρ is the resistivity of the earth in ohm-cm, L is the length of the conducting path, and A is the cross-sectional area of the path. Prof. H. B. Dwight of Massachusetts Institute of Technology developed rather complex formulas for the calculation of the resistance to earth for any distance from various systems of electrodes (Ref. 11). All such formulas can be simplified a little by basing them on the assumption that the earth's resistivity is uniform throughout the entire soil volume under consideration.

* An ohm-centimeter (abbreviated ohm-cm) is defined as the resistance of a cube of material (in this case, earth) with the cube sides being measured in centimeters.



Typical use of a Megger Null-Balance earth tester with digital read-out of measured earth resistance.

Because the formulas are complicated, and earth resistivity is neither uniform nor constant, a simple and direct method of measuring earth resistance is needed. This is where we come in with our Megger® earth tester — a self-contained portable instrument that is reliable and easy to use. With it, you can check the resistance of your earth electrode while it's being installed; and, by periodic tests, observe any changes with time.

To understand the principle of earth testing, consider the schematic diagram Fig. 5a. Bear in mind our previous observation with reference to the earth shell

diagram Fig. 4: with increased distance from an electrode, the earth shells are of greater surface area and therefore of lower resistance. Now, assume that you have three rods driven into the earth some distance apart and a voltage applied, as shown in Fig. 5a. The current between rods 1 and 2 is measured by an ammeter; the potential difference (voltage) between rods 1 and 3 is measured by a voltmeter.

If rod 3 is located at various points between rods 1 and 2, preferably in a straight line*, you can get a series of voltage readings. By Ohm's Law ($R = E/I$) you can determine the earth resistance at any point measured. For example, if the measured voltage E between rods 1 and 3 is 30 volts and the measured current I is 2 amperes, the resistance of the earth R at that point would be 15 ohms.

The series of resistance values can be plotted against distance to obtain a curve (Fig. 5b). Note that as rod 3 is moved away from rod 1, the resistance values increase but the amount of increase gets less and less until a point is reached where the rate of increase becomes so small that it can almost be considered constant (20 ohms in Fig. 5b). The earth shells between the two rods (1 and 3) have so great a surface area that they add little to the total resistance. Beyond this point, as rod 3 approaches the earth shells of rod 2, resistance gradually picks up. Near rod 2, the values rise sharply.

Now, let's say that rod 1 is our earth electrode under test. From a typical earth-resistance curve, such as Fig. 5b, what is the resistance to earth of this rod? We call rod 2 *current-reference probe* C_2 and rod 3, *potential-reference probe* P_2 (simply for convenience in identification—carried through on test instrument terminals). The correct resistance is usually obtained if P_2 (rod 3) is placed at a distance from the center of the earth electrode (rod 1) about 62% of the distance between the earth electrode and C_2 (rod 2).

For example, in Fig. 5b the distance D from the earth electrode to C_2 is 100 feet. Taking 62% of this distance, we get 62 feet. From Fig. 5b, the resistance for this distance is 20 ohms. This is the measured resistance of the earth electrode.

* Actually current can exist in other paths between the two fixed electrodes, so that rod 3 could (and might have to be) located at other than along a straight line.

This rule works well for simple electrodes, such as a driven rod. It also works for a small group of rods. But you must know the true electrical center of the electrode system fairly accurately. Also, accuracy of readings is better if the earth resistivity between the three electrodes is reasonably constant. Finally, C_2 should be far enough away from the earth-electrode system so that the 62% distance is out of the "sphere of influence" of the earth-electrode. (See discussion with reference to Figs. 8 and 9).

Basically, you now have the principle of earth-resistance testing. The rest is refinement—in test methods, use of electrodes or electrode systems, and information about earth resistivity, as covered in later portions of this manual.

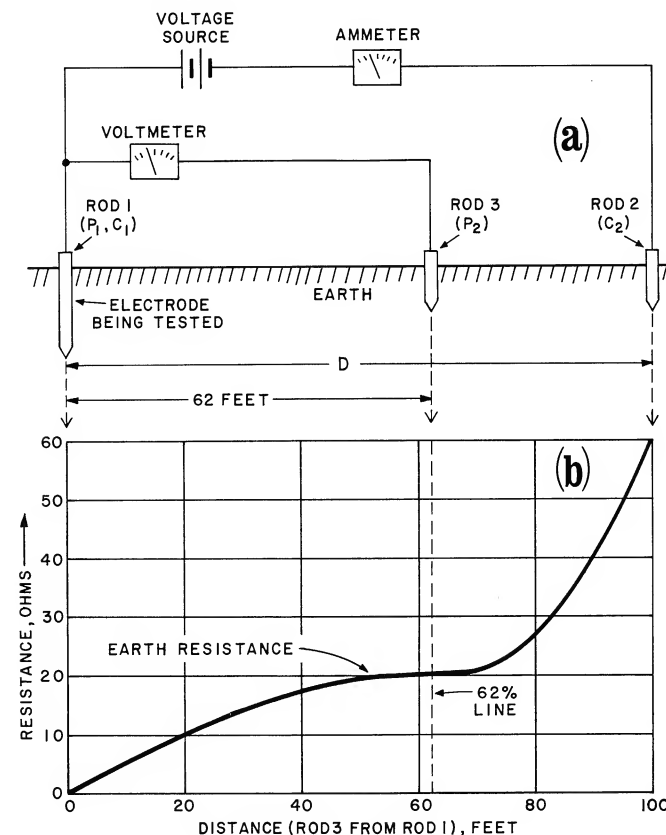


Fig. 5—Principle of an earth-resistance test.

BASIC TEST METHODS FOR EARTH RESISTANCE

Megger instruments for earth-resistance tests include: (1) a voltage source, (2) an ohmmeter to measure resistance directly, and (3) switches to change the instrument's resistance range. Extension wires connect four terminals (P_1 , C_1 , P_2 , C_2) on the instrument to the earth and reference electrodes, as will be described. A hand-cranked generator supplies the required current; you read resistance in ohms from a pointer on a scale or a digital read-out.

There are two basic test methods, shown schematically in Figs. 6 and 7, namely:

1. Direct Method, or Two-Terminal Test.
2. Fall-of-Potential Method, or Three-Terminal Test.

Direct Method: P_1 and C_1 terminals connect to the earth electrode under test; P_2 and C_2 terminals connect to an all-metallic water-pipe system (Fig. 6).

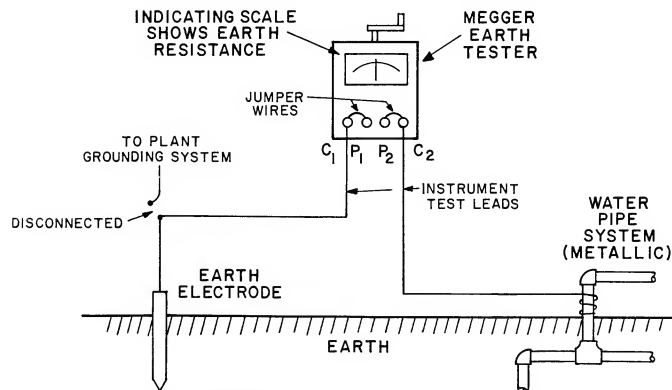


Fig. 6—"Direct Method" or "Two-Terminal" earth-resistance test.

If the water system is extensive (covering a large area), its resistance should only be a fraction of an ohm. You can then take the instrument reading as being the resistance of the electrode under test.

The Direct Method is the simplest way to make an earth-resistance test. With this method, resistance of two electrodes in series is measured—the driven rod and the water system. But there are three important limitations:

1. The water-pipe system must be extensive enough to have a negligible resistance.
2. The water-pipe system must be *metallic* throughout, without any insulating couplings or flanges.
3. The earth electrode under test must be far enough away from the water-pipe system to be outside its sphere of influence.

Rule of thumb: Distance from the earth-electrode system to the water-pipe system should be about 10 times the radius of the electrode or grid to obtain a measurement within an accuracy of $\pm 10\%$.*

In some locations, your earth electrode may be so close to the water-pipe system that you can not separate the two by the required distance for measurement by the two-terminal method. Under these circumstances, if conditions 1 and 2 above are met, you can connect to the water-pipe system and obtain a suitable earth electrode. As a precaution against any possible future changes in the resistance of the water-pipe system, however, you should also install an earth electrode.

Fall-of-Potential Method: This three-terminal test is the method described previously with reference to Fig. 5. The P_1 and C_1 terminals on the instrument are jumpered and connected to the earth electrode under test. The driven reference rod C_2 should be placed as far from the earth electrode as practical; this distance may be limited by the length of extension wire available, or the geography of the surroundings (see Fig. 7).

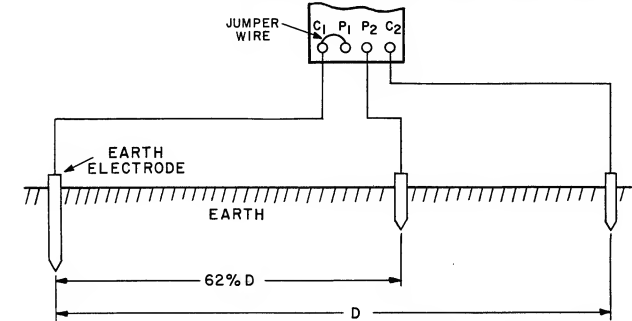


Fig. 7—"Fall-of-Potential" or "Three-Terminal" earth-resistance test.

* Such an accuracy is entirely adequate for this type of measurement. See Section II discussion on the variances of soil resistivity.

Potential-reference rod P_2 is then driven in at a number of points roughly on a straight line between the earth electrode and C_2 . Resistance readings are logged for each of the points. A curve of resistance vs distance, like Fig. 5b, is then drawn. Correct earth resistance is read from the curve for the distance that is about 62% of the total distance from the earth electrode to C_2 . In other words, if the total distance is D , the 62% distance is $0.62D$; for example, if D is 120 feet, the distance value for earth resistance is 0.62×120 or 74 feet.

EFFECTS OF DIFFERENT REFERENCE PROBE LOCATIONS

Now, you may ask: if the right location for probe P_2 is always 62% of the distance between the earth electrode and C_2 , why bother with all the tests at other locations for P_2 ? Why not just drive P_2 in at the 62% distance and assume that the measured resistance is the correct earth resistance? The following paragraphs should help answer these questions.

Minimum Distance for C_2 : Consider Fig. 8 which shows earth shells around the earth electrode and reference probe C_2 . In Fig. 8a, C_2 is so close to the earth electrode that the earth shells seriously overlap. Then you don't get the leveling off of measured resistance as P_2 is moved away from the earth electrode; the shells of C_2 add to the shells of the earth electrode. So the resistance keeps increasing.

In Fig. 8b, C_2 is placed farther away. Then the measured resistance levels off enough and at the 62% distance it is very close to the actual earth resistance. The reason for having C_2 farther away is to get assurance that the 62% value is "in line" with other values on the curve. The value could only be wrong (assuming there are no measuring mistakes) if the soil conditions at the 62% point vary from conditions at other points, causing changes in earth resistivity. You want to get some degree of flatness or leveling off of your curve to make such a variation easily noticeable.

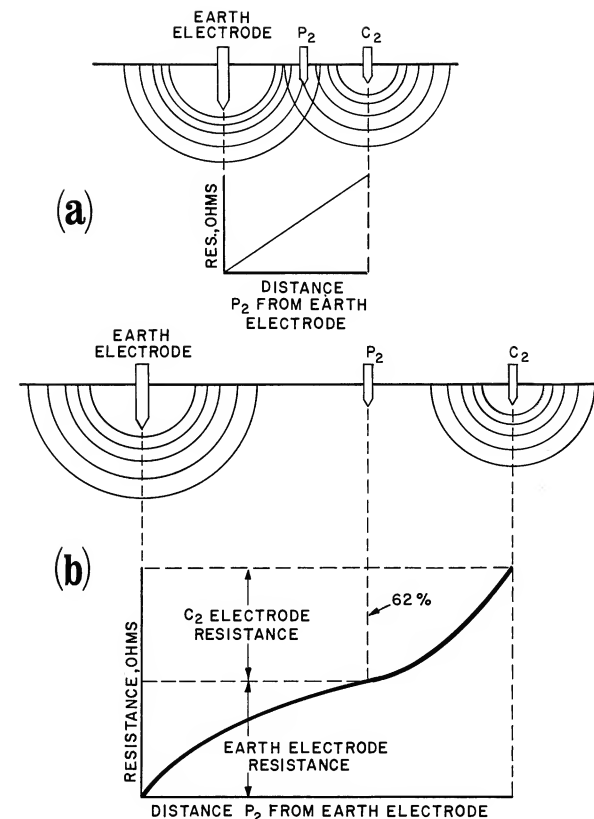
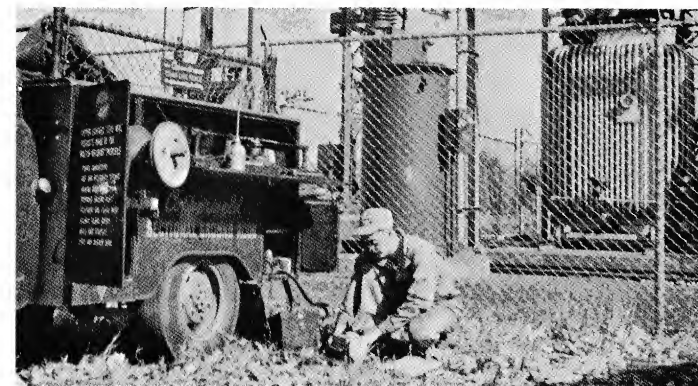


Fig. 8—Effect of C_2 location on the earth-resistance curve.



Photograph courtesy of Copperweld Steel Co.

Earth resistance being routinely checked from fully-equipped test truck.

As a practical example of this effect, consider the case illustrated in Fig. 9. This shows two earth-resistance curves for two locations of C_2 . Curve A was obtained when C_2 was 100 feet from the earth electrode; Curve B, when C_2 was 700 feet away. Curve A shows that C_2 was too close to the earth electrode; Curve B shows the desired tendency toward leveling out of the measured resistance. The 62% distance gives resistance values nearly the same in this case since the earth resistivity is fairly uniform.

Simplified Fall-of-Potential Test: Some users purposely do not place reference probe P_2 at the 62% distance. They use a procedure similar to that outlined under Fall-of-Potential Method, but they *start* with P_2 midway between the earth electrode and C_2 . After measuring the resistance for this point, they make two or three tests on either side about 10 feet apart. If the midpoint resistance agrees with the other readings within required accuracy, the mean value is used as the earth resistance.

If the readings are not within the required accuracy, probe C_2 has to be placed farther away and the tests repeated. This method can give sufficient accuracy, but will always give values on the low side. (See discussion following with reference to Table I.)

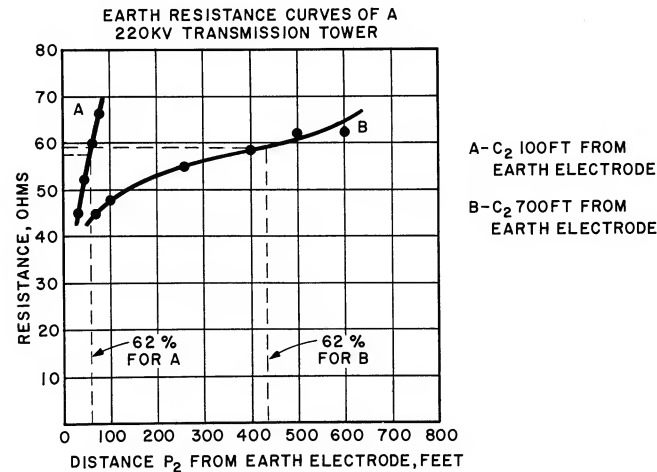


Fig. 9—Example of how C_2 location affects the earth-resistance curve.

Some Rules of Thumb on Spacing P_2 and C_2 : With a small grid of one or two earth electrodes, C_2 can usually be placed about 100 to 125 feet from the electrode under test; P_2 correspondingly can be placed about 62 to 78 feet away. If the earth electrode is large—consisting, for example, of several rods or plates in parallel—the distance for C_2 must be increased to possibly 200 feet, and for P_2 to some 125 feet. You'll need even greater distance for complex electrode systems that consist of, say, a large number of rods or plates and other metallic structures—all bonded together.

Table I is a useful guide to reference probe location. You find the "Maximum Dimension" figure by taking the diagonal distance across your electrode system area. For example, if the area measures 100 by 100 feet, the diagonal equals about 140 feet. From the table, you run down the first column to 140 and read across that P_2 should be 365 feet from the electrode and C_2 , 590 feet.

TABLE I—Guide to Approximate Location of Reference Probes (See Note 1)

MAXIMUM DIMENSION, FT. (See Note 2)	DISTANCE TO P_2 , FT.	DISTANCE TO C_2 , FT.
2	40	70
4	60	100
6	80	125
8	90	140
10	100	160
12	105	170
14	120	190
16	125	200
18	130	210
20	140	220
40	200	320
60	240	390
80	280	450
100	310	500
120	340	550
140	365	590
160	400	640
180	420	680
200	440	710

Note 1—Based upon data in Reference 2.

Note 2—For example, the diagonal across an area surrounded by an earthed fence.

HOW TO IMPROVE EARTH RESISTANCE

When you find that your earth-electrode resistance is not low enough, there are several ways you can improve it:

1. Lengthen the earth electrode in the earth
2. Use multiple rods
3. Treat the soil.

Effect of Rod Size: As you might suspect, driving a longer rod deeper into the earth, materially decreases its resistance. In general, *doubling the rod length reduces resistance by about 40%*. The curve of Fig. 10 shows this effect. For example, note that a rod driven two feet down has a resistance of 88 ohms; the same rod driven 4 feet down has a resistance of about 50 ohms. Using the 40% reduction rule, $88 \times 0.4 = 35$ ohms *reduction*. A 4-foot deep rod, by this calculation would have a resistance of $88 - 35$ or 53 ohms—comparing closely with the curve values.

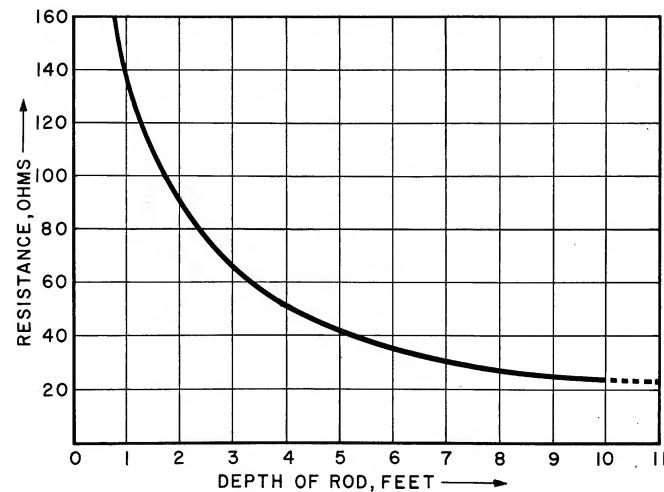


Fig. 10—Earth resistance decreases with depth of electrode in earth. (Source: Reference 19)

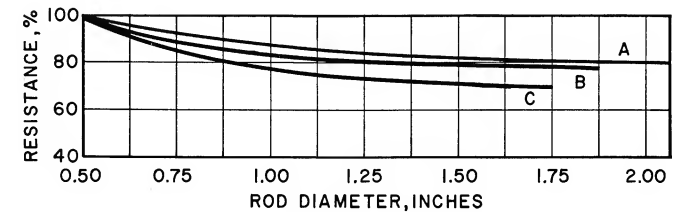


Fig. 11—Diameter of a rod has little effect on its earth resistance.

Curve A, from Reference 19.

Curve B, average of Underwriters Laboratories tests at Chicago.

Curve C, average of Underwriters Laboratories tests at Pittsburgh.

You might also think that increasing the electrode diameter would lower the resistance. It does, but only a little. For the same depth, doubling the rod's diameter reduces the resistance only about 10%. Fig. 11 shows this relationship. For example, a 10-foot deep rod, $\frac{5}{8}$ inch in diameter, has a resistance of 6.33 ohms; increasing its diameter to $1\frac{1}{4}$ inch lowers the resistance only to 5.6 ohms. For this reason, you normally only consider increasing the rod diameter if you have to drive it into hard terrain.

Use of Multiple Rods: Two well-spaced rods driven into the earth provide parallel paths. They are, in effect, two resistances in parallel. The rule for two resistances in parallel does not apply exactly; that is, the resultant resistance is not one-half the individual rod resistances (assuming they are of the same size and depth). Actually, the reduction for two equal-resistance rods is about 60%. If three rods are used, the reduction is 40, and if four, 33% (see Fig. 12).

When you use multiple rods, they must be spaced apart further than the length of their immersion. There are theoretical reasons for this, but you need only refer to curves such as Fig. 13. For example, if you have two rods in parallel and 10-foot spacing, resistance is lowered about 60%. If the spacing is increased to 20 feet, reduction is about 50%.

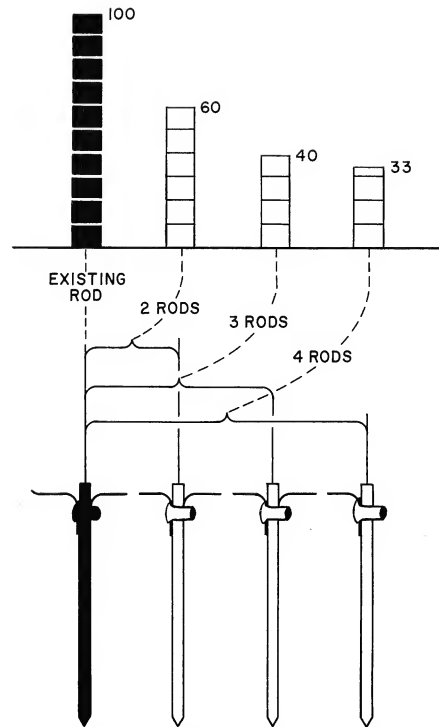


Fig. 12—Average results obtained from multiple-rod earth electrodes.*

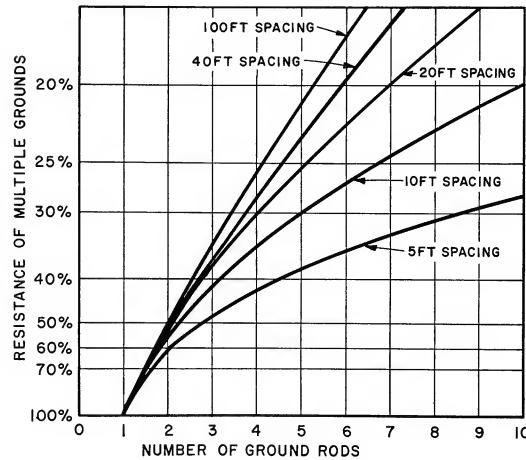


Fig. 13—Comparative resistance of multiple-rod earth electrodes. Single rod equals 100%.*

* Source: Reference 20

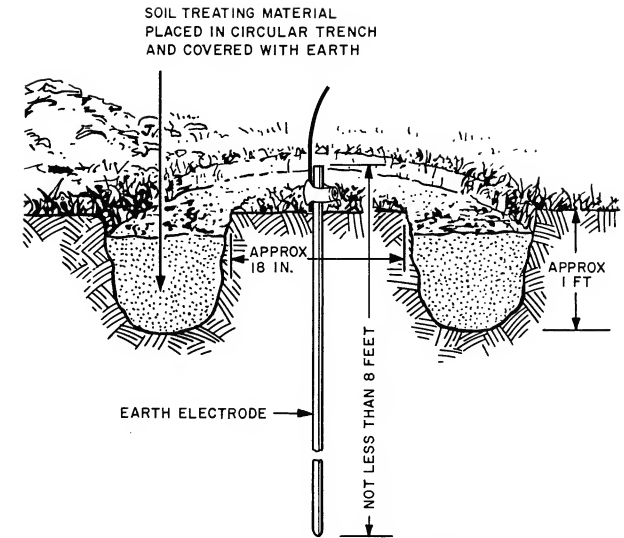


Fig. 14—Trench method of soil treatment.*

Treatment of the Soil: Chemical treatment of soil is a good way to improve earth-electrode resistance when you can't drive deeper ground rods—because of hard underlying rock, for example. It is beyond the scope of this manual to recommend the best treatment chemicals for all situations. You have to consider the possible corrosive effect on the electrode. Magnesium sulfate, copper sulfate, and ordinary rock salt are suitable non-corrosive materials. Magnesium sulfate is the least corrosive, but rock salt is cheaper and does the job if applied in a trench dug around the electrode. (Fig. 14).

Chemical treatment is not a permanent way to improve your earth-electrode resistance. The chemicals are gradually washed away by rainfall and natural drainage through the soil. Depending upon the porosity of the soil and the amount of rainfall, the period for replacement varies. It may be several years before another treatment is required.

* Source: Reference 20

Chemical treatment also has the advantage of reducing the seasonal variation in resistance that results from periodical wetting and drying out of the soil. (See curves of Fig. 15). However, you should only consider this method when deep or multiple electrodes are not practical.

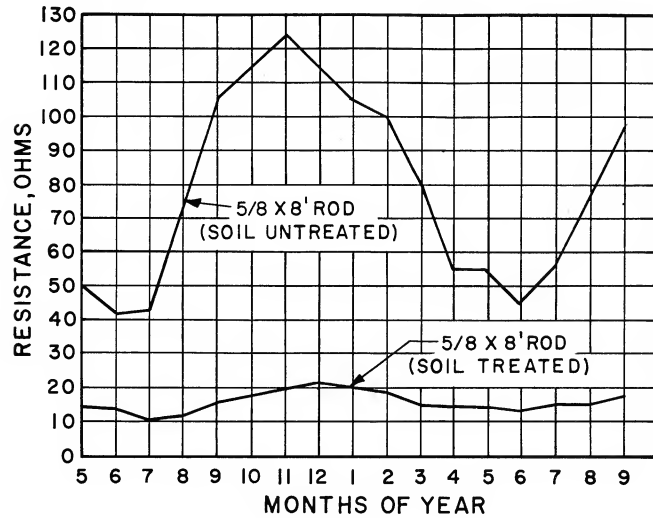


Fig. 15—Chemical treatment of soil lessens seasonal variation of electrode's earth-resistance.*

* Source: Reference 20

SECTION II

Earth Resistivity

As we've seen in Section I, the term, "earth resistivity", expressed in *ohm-centimeters* (abbreviated *ohm-cm*), is one basic variable affecting resistance to earth of an electrode system. But you found that the actual value of earth resistivity need not be measured to check the electrode earth resistance. Now we'll consider other fields where the value of resistivity is measured; also some of the factors affecting it that are of interest in earth testing.

Earth resistivity measurements can be used conveniently for geophysical prospecting—to locate ore bodies, clays, and water bearing gravel beneath the earth's surface. The measurement can also be used to determine depth to bed rock and thickness of glacial drift.

Measurements of earth resistivity are useful also for finding the best location and depth for low-resistance electrodes. Such studies are made, for example, when a new electrical unit is to be constructed—a generating station, sub-station, transmission tower, or telephone central office.

Finally, earth resistivity may be used to indicate the degree of corrosion to be expected in underground pipelines for water, oil, gas, gasoline, etc. In general, spots where the resistivity values are low tend to increase corrosion. This same kind of information is a good guide for installing cathodic protection.

HOW EARTH RESISTIVITY IS MEASURED

The same Megger instrument that you use to measure earth-electrode resistance is used to measure earth resistivity. Now, however, you use *four* small-sized electrodes *driven down the same amount and equal distances apart* in a straight line (Fig. 16). Four separate lead wires connect the electrodes to the four terminals on the instrument, as shown. Hence the name of this test: *the four-terminal method*.

Dr. Frank Wenner of the U. S. Bureau of Standards developed the theory behind this test in 1915 (see reference 10). He showed that, if the electrode depth (B) is kept small compared to the distance between the electrodes (A)*, the following formula applies:

$$\rho = 2\pi AR$$

where ρ is the average soil resistivity to depth A in ohm-cm, π is the constant 3.1416, A is distance between the electrodes in cm, and R is the Megger instrument reading in ohms.

In other words, if the distance A between electrodes is 4 feet, you obtain the average earth resistivity to a depth of 4 feet as follows:

1. Convert the 4 feet to centimeters to obtain A in the formula:
 $4 \times 12 \times 2.54 \text{ cm} = 122 \text{ cm}$
2. Multiply $2\pi A$ to obtain a constant for a given test set-up:
 $2 \times 3.14 \times 122 = 766$

Now, for example, if your instrument reading is 60 ohms, the earth resistivity would be 60×766 , or 45,960 ohm-cm.

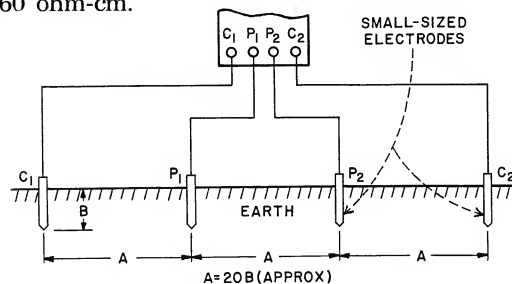


Fig. 16—"Four-Terminal" method of measuring earth resistivity.

* $B = 1/20A$ is generally recommended.

PRACTICAL EXAMPLE OF TEST METHOD*

A petroleum company had a 10-inch pipeline 6300 feet long running through rugged terrain. After a corrosion leak, they wanted to check out earth resistivity along the line. Low-resistance spots would most likely require attention. So they used a Megger instrument to make a survey along the line.

First, average depth of the pipeline was found from a profile map. It was four feet, so the four electrodes were tied together 4 feet apart with strong cotton cord. They decided to check soil resistivity every 20 feet along the line. Fig. 17 shows a portion of the results; pit depth of corrosion and Megger instrument readings are both plotted for points along the pipeline. Note that for low resistance readings, more corrosion was found.

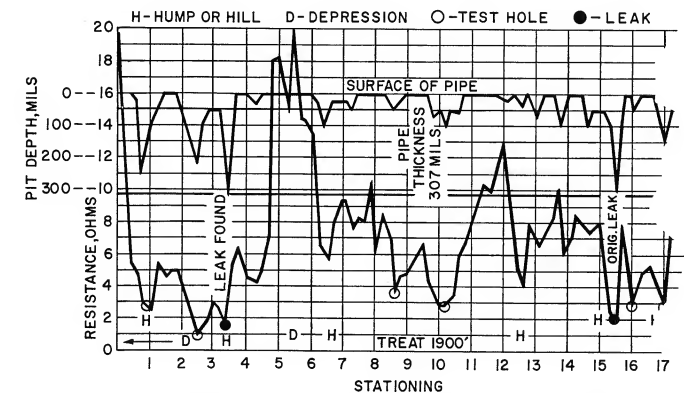


Fig. 17—Earth-resistivity survey of pipeline shows where corrosion is most likely to occur. (Source: Reference 18)

* Reference 18

TYPE OF SOIL AFFECTS RESISTIVITY

Whether a soil is largely clay or very sandy, for example, can change the earth resistivity very much. It isn't easy to define exactly a given soil; "clay" can cover a wide variety of soils. So we can't say that any given soil has a resistivity of so many ohm-cm. Accompanying Tables II and III from two different reference books show the wide range in values. Note also the spread of values for the same general types of soil. See also Fig. 18 on page 33.

TABLE II—Resistivities of Different Soils*

SOIL	RESISTIVITY OHM-CM		
	AVERAGE	MIN.	MAX.
Fills—ashes, cinders, brine wastes	2,370	590	7,000
Clay, shale, gumbo, loam	4,060	340	16,300
Same—with varying proportions of sand and gravel	15,800	1,020	135,000
Gravel, sand, stones, with little clay or loam	94,000	59,000	458,000

* U. S. Bureau of Standards Technical Report 108

TABLE III—Resistivities of Different Soils**

SOIL	RESISTIVITY, OHM-CM (RANGE)
Surface soils, loam, etc.	100 — 5,000
Clay	200 — 10,000
Sand and gravel	5,000 — 100,000
Surface limestone	10,000 — 1,000,000
Limestones	500 — 400,000
Shales	500 — 10,000
Sandstone	2,000 — 200,000
Granites, basalts, etc.	100,000
Decomposed gneisses	5,000 — 50,000
Slates, etc.	1,000 — 10,000

** Evershed & Vignoles Bulletin 245.

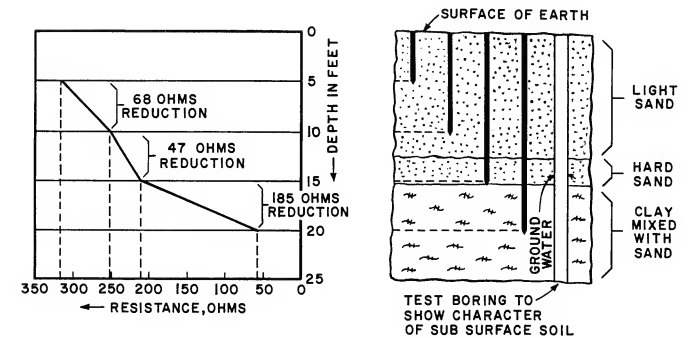


Fig. 18—Deeper earth electrodes lower the resistance. These graphs show the relation between character of soil and resistance of driven electrode at increased depths.

RESISTIVITY DECREASES WITH MOISTURE AND DISSOLVED SALTS

In soil, conduction of current is largely electrolytic. So the amount of moisture and salt content of soil radically affect its resistivity. Amount of water in soil varies, of course, with the weather, time of year, nature of sub-soil, and depth of the permanent water table. The accompanying Table IV shows typical effects of water in soil; note that when dry the two types of soil are good insulators (resistivities greater than 1000×10^6 ohm-cm). With a moisture content of 15%, however, note the drastic decrease in resistivity (by a factor of about 100,000).

TABLE IV—Effect of Moisture Content on Earth Resistivity +

MOISTURE CONTENT, % BY WEIGHT	RESISTIVITY, OHM-CM	
	TOP SOIL	SANDY LOAM
0	$1,000 \times 10^6$	$1,000 \times 10^6$
2.5	250,000	150,000
5	165,000	43,000
10	53,000	18,500
15	1,000	10,500
20	12,000	6,300
30	6,400	4,200

+ From "An Investigation of Earthing Resistance", by P. J. Higgs, I.E.E.E. Jour., vol. 68, p. 736, February 1930.

Actually, pure water has an infinitely high resistivity. Naturally-occurring salts in the earth, dissolved in water, lower the resistivity. Only a small amount of a salt* can reduce earth resistivity quite a bit (see Table V). As we noted in Section I, this effect can be useful to provide a good low-resistance electrode, in place of an expensive, elaborate electrode system.

TABLE V—Effect of Salt Content on Earth Resistivity**

ADDED SALT % BY WEIGHT OF MOISTURE	RESISTIVITY, OHM-CM
0	10,700
0.1	1,800
1.0	460
5	190
10	130
20	100

** For sandy loam—moisture content, 15% by weight; temperature, 17°C (63°F).

EFFECT OF TEMPERATURE ON EARTH RESISTIVITY

Not much information has been collected on the effects of temperature. Two facts lead to the logical conclusion that an increase in temperature will decrease resistivity: (1) water present in soil mostly determines the resistivity, and (2) an increase in temperature markedly decreases the resistivity of water. The results shown in Table VI confirm this. Note that when water in the soil freezes, the resistivity jumps appreciably;

TABLE VI—Effect of Temperature on Earth Resistivity†

TEMPERATURE		RESISTIVITY, OHM-CM
C	F	
20	68	7,200
10	50	9,900
0	32 (water)	13,800
0	32 (ice)	30,000
- 5	23	79,000
-15	14	330,000

† For sandy loam, 15.2% moisture.

* By "salt" we mean not just the kind you use to season food (sodium chloride) though this kind can occur in the soil. Other kinds include copper sulphate, sodium carbonate, and others (see "Treatment of Soil", Section I, P. 27).

ice has a high resistivity. Note also that the resistivity continues to increase as temperatures go below freezing. You could have a really-high value at the North Pole!

From the table, note that a 54-degree drop in temperature (from 68°F to 14°F) causes almost a 50-fold increase in resistivity.

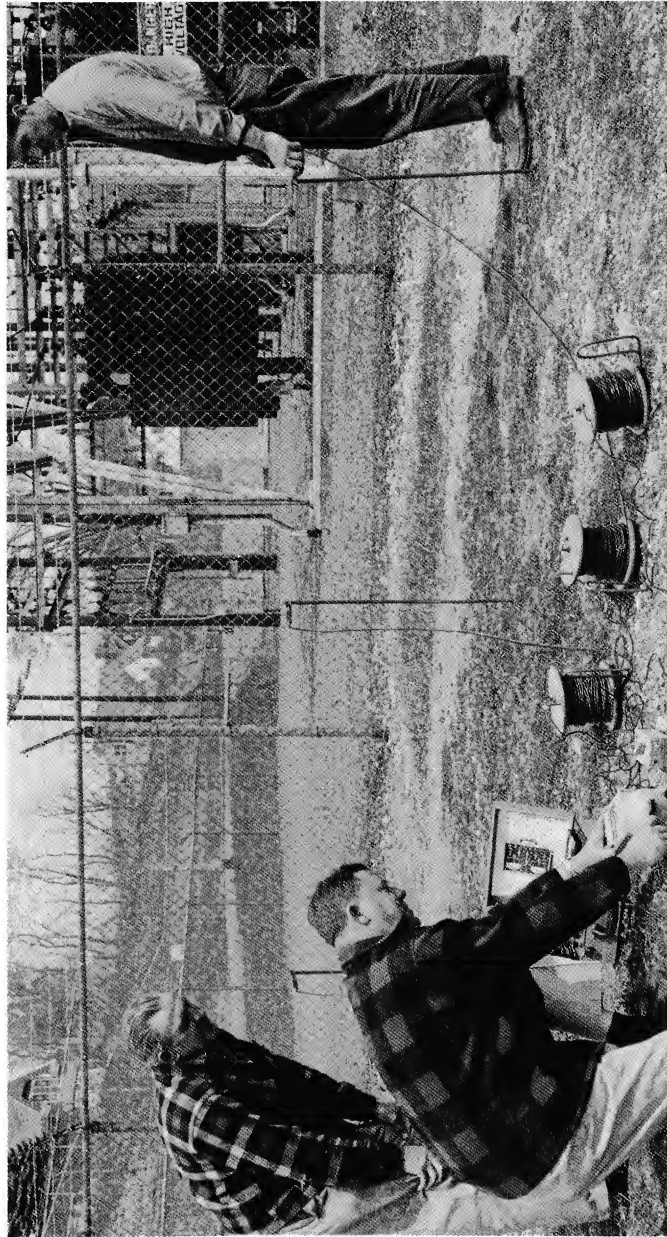
SEASONAL VARIATIONS IN EARTH RESISTIVITY

We have seen the effects of temperature, moisture, and salt content upon earth resistivity. It makes sense, therefore, that the resistivity of soil will vary considerably at different times of the year. This is particularly true in locations where there are more extremes of temperature, rainfall, dry spells, and other seasonal variations.



Photograph courtesy of Messinger Bearing Co.

A three-terminal earth-resistance test being made at an industrial transformer installation.



Photograph courtesy of Worcester County Electric Co.

Utility uses Megger tester on underground cable system to spot area of low earth resistivity to stray electrical currents. Correcting such spots in time prevents electrolytic corrosion.

From all the preceding discussion, you can see that earth resistivity is a very variable quantity. If you want to know what the value is at a given location, at a given time of the year, the only safe way is to measure it. When you use this value for survey work, the *change* in the value, caused by changes in the nature of the sub-soil, is the important thing; from the variations in resistivity you can obtain useful survey results.

As covered in Section I, the other main reason for being interested in earth resistivity is to design earth-electrode systems for electrical power systems, lightning arresters, and so on. Earth resistance varies directly with earth resistivity and it's helpful to know what factors affect resistivity.

The curves of Fig. 19 illustrate several worthwhile points. They show the expected change in earth resistance (due to resistivity changes) over a 1½-year period; they also show that the deeper electrode gives a more stable and lower value. We conclude that the moisture content and temperature of the soil become more stable at greater distances below the earth's surface. Therefore, the earth electrode, should reach a deep enough level to provide:

1. Permanent moisture content (relatively speaking)
2. Constant temperature (below frost line; again relatively speaking).

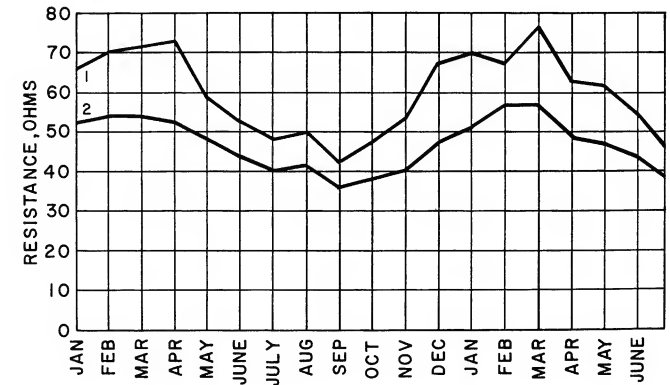


Fig. 19—Seasonal variation of earth resistance with an electrode of ¾-inch pipe in rather stony clay soil. Depth of electrode in earth is 3 ft for Curve 1, and 10 ft for Curve 2. (Source: Reference 9)

DETERMINING A GOOD ELECTRODE LOCATION

A good, low-resistance earth electrode depends upon a low-resistivity soil in a spot where you can drive in your electrodes. There are two approaches to picking your location:

1. Drive rods in various locations to such depths as may be required and test their resistances while they are being driven.
2. Measure the earth resistivity *before* driving ground rods. Then calculate the number and length of rods required.

To get a low-resistance electrode in an unfavorable location, lay out straight lines 10 feet apart, covering the area. Drive four stakes 10 feet apart, but not more than six inches deep, along a line a-b-c-d, as shown in Fig. 20. Measure the resistance R between stakes b and c, using the method described for earth resistivity.

Then, shift the stakes along the line in question to points b-c-d-e, c-d-e-f, and so on (see Fig. 20) and test until the entire line has been covered. Next, move to the next line and repeat the process until the whole chosen area has been covered. The location giving the lowest value for R has the lowest specific resistance for the soil to the chosen depth of 10 feet. The spot is likely to give you the best earth electrode.

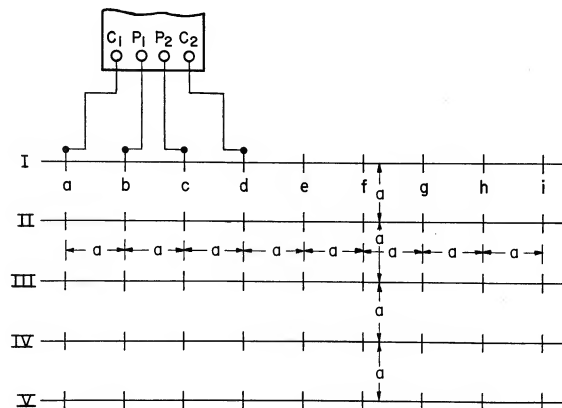
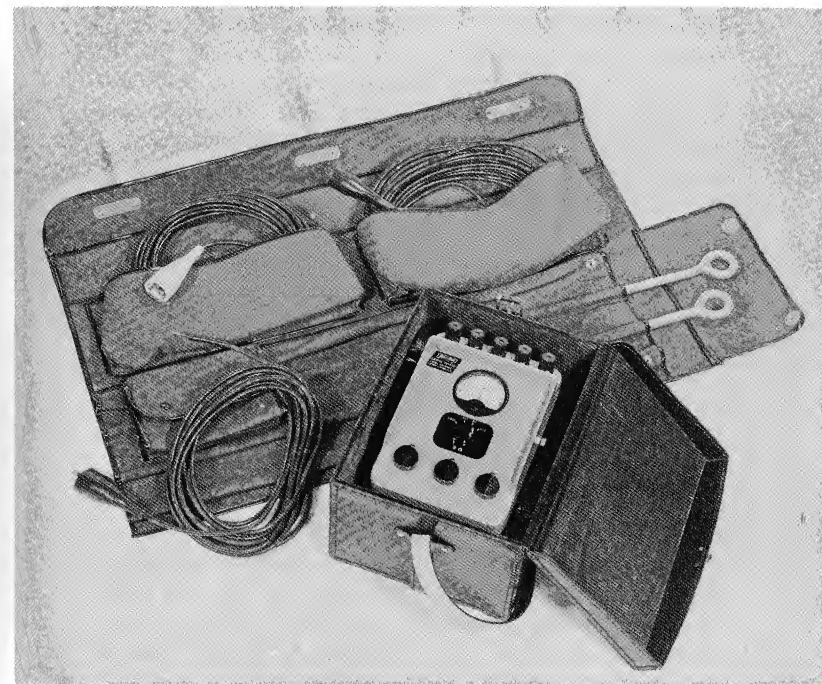


Fig. 20—Method of prospecting for best earth electrode location to a depth a . Location giving lowest reading on the Megger earth tester is the most desirable.

If you want results affected by the average earth resistivity to a depth of 20 feet, repeat the survey on lines 20 feet apart and with stakes spaced 20 feet apart. Such surveys do not require much time and can pay off in assuring a good grounding system.

Alternate Method: Another way is to drive rods or pipes in various locations to such depths as may prove practicable, testing their resistance *while they are being driven*. In this manner, you can usually tell at once when moisture or other good conducting earth is reached. However, the work involved is apt to be much more than with the first method.



Typical earth-resistance test kit with ground rods and cable, plus a Megger Null-Balance instrument in carrying case.

NOMOGRAPH GUIDE TO SETTING ACCEPTABLE EARTH RESISTANCE

Dr. L. E. Whitehead of the DuPage Laboratories developed a nomograph (Fig. 21) which can be a helpful guide in meeting the established standard for a minimum earth resistance. If you have a given earth-electrode system and find that your Megger instrument reading is too high, the graph can be used to show what you must do to lower the value. Note that it covers three variable conditions that affect earth resistance of the electrode: *earth resistivity, length of rod, and diameter of rod.*

To illustrate use of the nomograph, let's take an example. Assume you have a $\frac{5}{8}$ -inch rod driven 10 feet into the soil. Your Megger instrument indicates an earth resistance of 6.6 ohms. But let's say your specification for this resistance is "no more than 4 ohms." To get this, you can change one or more of the three variables; the simplest and most effective being depth of the driven rod. To find the required depth to give you a 4-ohm earth resistance, proceed as follows: With a ruler, draw a line from the 10-foot point in the *L* line to the $\frac{5}{8}$ -inch point in the *d* line; this gives a reference point where the line crosses the *q* line. Connect this reference point with 6.6 ohms—the measured resistance on the *R* line, as shown in Fig. 21, read the value of earth resistivity where this line crosses the ρ line. The value is 2000 ohm-cm.

To determine the required rod depth for a 4-ohm earth resistance, draw a line from this point on the *R* line through the 2000 point on the line until you cross the *q* line. The dashed line on Fig. 21 shows this step. Now, assuming you keep rod diameter unchanged, connect the $\frac{5}{8}$ point on *d* line through your new reference point on *q* and extend the line to *L*. This gives you the required rod depth for the 4-ohm resistance value. Finally, take a new instrument reading to check the value, because earth resistivity may not be constant (as the nomograph assumes).

Another way to reduce the earth resistance would be to lower the earth resistivity. Note in Fig. 21 that if you draw a line from a reference point 1 (leaving rod depth and diameter unchanged), you would need

to reduce earth resistivity to about 1000 ohm-cm to give the required 4-ohm earth resistance. You could do this by chemical treatment, as described earlier, but normally the deeper rod is the easier way.

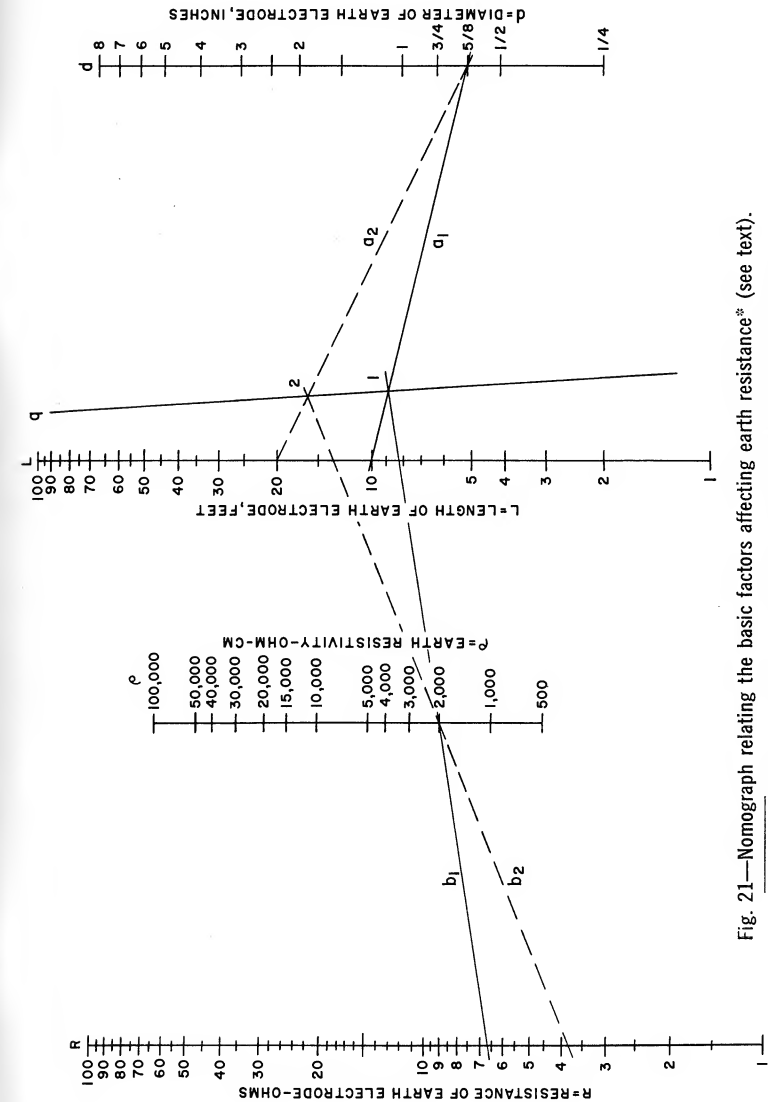


Fig. 21—Nomograph relating the basic factors affecting earth resistance* (see text).

* Adapted from nomograph published in an article, "Nomograph Determines Ground-Rod Resistance," L. E. Whitehead, Electric Light & Power, December 1962.

REFERENCES

1. "Earth Conduction Effects in Transmission System," E. D. Sunde, D. Van Nostrand Co.
2. "Earth Resistances," G. F. Tagg, George Newnes Limited, London (1964).
3. "Principles and Practices in Grounding," Pub. No. D9, Edison Electric Institute.
4. "Guide for Safety in Alternating-Current Substation Grounding," AIEE (IEEE) No. 80.
5. "Recommended Guide for Measuring Ground Resistance and Potential Gradients in the Earth." AIEE (IEEE) No. 81.
6. "Master Test Code for Resistance Measurement, AIEE (IEEE) No. 550.
7. "Some of the Fundamental Aspects of Ground Resistance Measurements, E. B. Curdts, AIEE (IEEE) Paper No. 58-106, Transactions, Vol. 77, 1958
8. "Equipment Grounding," Industrial Power System Data Book, General Electric Co.
9. "Grounding Electric Circuits Effectively," J. R. Eaton, GENERAL ELECTRIC REVIEW, June, July, August 1941 (Biddle Bulletin 25T2).
10. "A Method of Measuring Earth Resistivity," F. Wenner, Report No. 258, Bulletin of Bureau of Standards, Vol. 12, No. 3, Oct. 11, 1915.
11. "Calculation of Resistance to Ground," H. B. Dwight, AIEE (IEEE) Transactions, Vol. 55, 1936.
12. "Lightning Arrester Grounds," H. M. Towne, GENERAL ELECTRIC REVIEW, Parts I, II, III, Vol. 35, pp. 173, 215, 280, March, April, May 1932.
13. "Grounding Principles and Practices-Fundamental Considerations on Ground Currents," R. Rudenberg AIEE (IEEE), ELECT. ENG., January 1946, also AIEE (IEEE) Publication S2.
14. "Grounding Principles and Practices—Establishing Grounds," C. H. Jensen, AIEE (IEEE), ELECT. ENG., February 1945, also AIEE (IEEE) Publications S2.
15. "Deep Driven Grounds," C. H. Jensen, EEI, T&D Committee, May 1951.
16. "Grounding Principles and Practices—Static Electricity in Industry," Beach, AIEE (IEEE) Publication S2.
17. "Corrosion of Buried Metals and Cathodic Protection," M. C. Miller, PETROLEUM ENGINEER, March, April, May, June 1944.
18. "An Experience With The Megger," W. H. Simpson, OIL AND GAS JOURNAL.
19. "Ground Connections for Electrical Systems," O. S. Peters, U. S. National Bureau of Standards, Technological Paper 108, June 20, 1918 (224 pages—now out of print).
20. "Practical Grounding Principles and Practices for Securing Safe Dependable Grounds," Publication of Copperweld Steel Co., Glassport, Pa.

NOTES

NOTES

NOTES

NOTES

BIDDLE

Instruments for Industry

- Megger® Insulation Testers, Heavy
Duty Types (21-20)
- Meg® Type of Megger Insulation
Testers (21-45)
- Multi-Purpose Major Megger Tester (21-50)
- Mark III Type of Megger Insulation
Testers (21-85)
- Transistorized Battery Megger
Tester (21-86)
- Bridge-Meg—Wheatstone Bridge and
Insulation Tester (21-60)
-
- Biddle 5 kv Dielectric Test Set (22-5)
- Biddle 15 kv Dielectric Test Set (22-15)
- Biddle 40 kv Dielectric Test Set (22-40)
- Biddle 100 kv Dielectric Test Set (22-100)
-
- Megger Earth Tester—Null Balance (25-40)
- Megger Ground Testing Instruments (25a)
-
- Ducter® Low Resistance Ohmmeter (24-25)
- Transformer Turn Ratio (TTR) Test Set (55)
- Biddle Cable Fault Locators (65)
- Motor Rotation and Phase Tester (80)
- Biddle Corona Test Equipment (66)
-
- Portable Wheatstone Bridges and
Test Sets (60-04)
- Portable Potentiometer (60-36)
-
- Speed Measuring Instruments—
Chronometric, centrifugal, and
resonant reed types for hand use
and permanent mounting (35)
- Biddle Electric Tachometers (31-32)



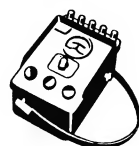
MEG-TYPE MEGGER
INSULATION TESTER



MAJOR
MEGGER TESTER



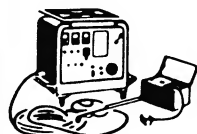
BIDDLE DIELECTRIC
TEST SET



MEGGER NULL BALANCE
EARTH TESTER



"TTR" TRANSFORMER
TURN RATIO TEST SET



BIDDLE IMPULSE CABLE
FAULT LOCATION EQUIPMENT



CORONA TEST
EQUIPMENT

MAIL POSTAGE PAID REPLY CARD

for information on
Biddle Instruments for Industry

NOTE: If both reply cards have been used, address your request to:
James G. Biddle Co., Plymouth Meeting, Pa. 19462, giving item
numbers desired.

Date _____

Gentlemen:

Please send me literature on items circled below:

21-20	21-86	22-40	24-25	66
				60-04
21-45	21-60	22-100	55	60-36
21-50	22-5	25-40	65	35
21-85	22-15	25a	80	31-32

Other requests _____

NAME _____ TITLE _____

COMPANY _____

CITY _____ STATE _____ ZIP _____

Date _____

Gentlemen:

Please send me literature on items circled below:

21-20	21-86	22-40	24-25	66
				60-04
21-45	21-60	22-100	55	60-36
21-50	22-5	25-40	65	35
21-85	22-15	25a	80	31-32

Other requests _____

NAME _____ TITLE _____

COMPANY _____

CITY _____ STATE _____ ZIP _____

**FOR MORE
INFORMATION**

(SEE REVERSE SIDE)

BUSINESS REPLY MAIL

No Postage Stamp Necessary if Mailed in the United States

Postage will be paid by

JAMES G. BIDDLE CO.
PLYMOUTH MEETING,
PENNSYLVANIA 19462

BUSINESS REPLY MAIL

No Postage Stamp Necessary if Mailed in the United States

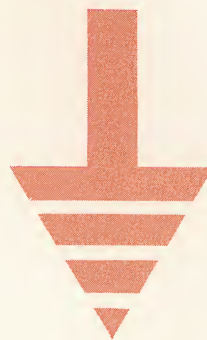
Postage will be paid by

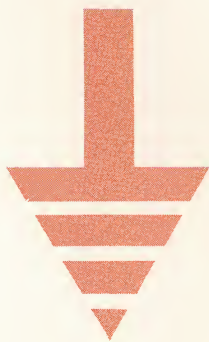
JAMES G. BIDDLE CO.
PLYMOUTH MEETING,
PENNSYLVANIA 19462

FIRST CLASS
PERMIT NO. 31
PLYMOUTH MEETING, PA.



FIRST CLASS
PERMIT NO. 31
PLYMOUTH MEETING, PA.







MEGGER® EARTH TESTERS

*... for measuring
resistance of earth
to ground connections
and for determining
earth resistivity*

A Megger Earth Tester measures the resistance to earth of ground connections simply, easily and accurately, thereby helping to determine whether such connections will perform the services for which they were intended. Earth resistivity determinations may also be made with greater ease with these instruments.

GROUND RESISTANCE

Grounding surveys have shown conclusively that for protection to life and property and for the correct functioning of nearly all types of electrical equipment—especially lightning arresters, distribution transformers, and equipment in sub-stations—much depends on suitable and permanent ground connections. This includes the electrical connections from machine frames, transformer cases, cable sheaths, metal housings, etc., to the earth connections, as well as the earth connections themselves.

EARTH RESISTIVITY

Megger Earth Testers provide, in addition to ground resistance measurements, a highly convenient means for measuring resistance values required for earth resistivity determinations.

Geophysical Prospecting

Earth resistivity measurements constitute one of the electrical methods for geophysical prospecting for ore bodies, clays and water bearing gravels and for other determinations such as depth to bed rock and thickness of glacial drift.

Electrical Power and Communications Problems

Measurements of earth resistivity can be used for determining quickly and easily the best locations and depths for high capacity and low resistance connections. Such studies can be helpful in determining the best location for installation of generating station, sub-station, transmission tower and telephone central office grounds.

Soil Corrosion—Electrolysis—Cathodic Protection

The Megger Earth Tester offers a convenient and relatively inexpensive means for studying the electrical characteristics of soil in relation to corrosion of water, oil, gas and gasoline pipelines, and for determining the locations where corrosion is most likely to occur.



JAMES G. BIDDLE CO.

Electrical Testing & Speed Measuring Instruments

Plymouth Meeting, Pennsylvania 19462

MEGGER® UNIVERSAL MULTI-RANGE EARTH TESTER

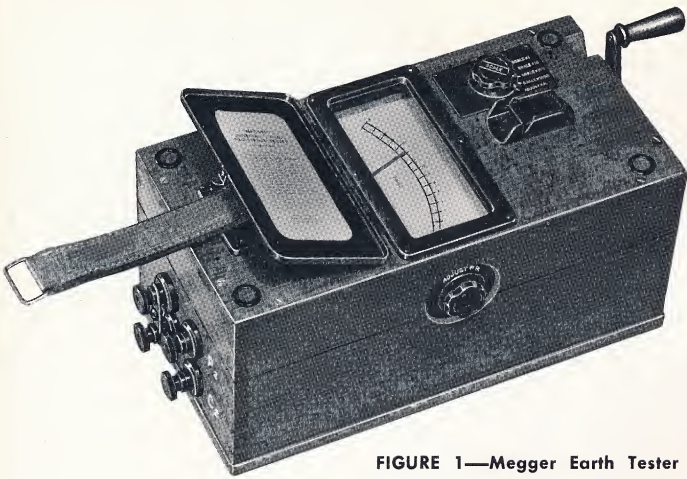


FIGURE 1—Megger Earth Tester 601

The outstanding performance records and proven dependability, associated with Megger instruments for over 50 years, are pronounced features of the new design now available in the Megger Universal Earth Tester.

The new model, replacing four old models, has ranges of 0 to 20, 0 to 200, 0 to 2000 and 0 to 20,000 ohms.

The new features include:

LONGER, MORE OPEN SCALE

The 30% longer scale (approximately 5") is logarithmic in character, permitting closer readings within each scale division. One ohm extends over 1/3 of scale on first range.

COMPENSATED FOR EXTERNAL POTENTIAL PROBE RESISTANCES UP TO 8000 OHMS CONVENIENT, SIMPLE ADJUSTMENT

The control knob for compensating potential probe resistances up to 8000 ohms is placed conveniently on the side of the instrument facing operator.

EASY OPERATION

The generator has a long, easy-to-turn crank handle. These instruments are housed in sturdy teakwood cases designed to withstand hard use and protect the instrument from damage due to rough handling and weather.

A comfortable leather grip makes these 22-pound instruments easily portable and ideal for hard, extensive field use. The overall dimensions are 14" x 7" x 7".

For Specifications see Page 4.

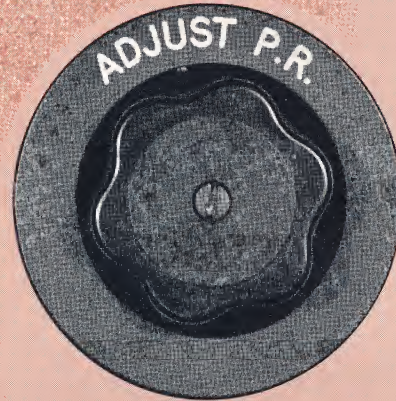


FIGURE 2—Full size view of Adjust P.R. control knob of the rheostat which compensates for external potential probe resistances up to 8000 ohms.

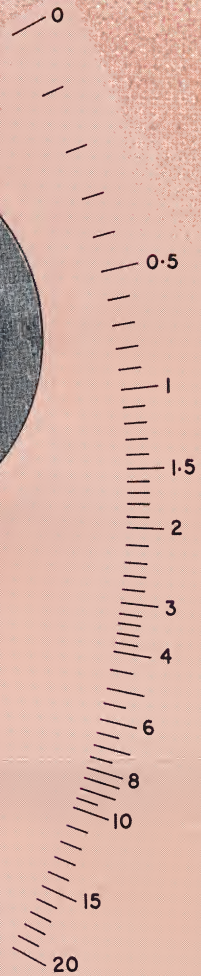


FIGURE 3—Facsimile scale, logarithmic in character, showing the 1 ohm position at about 1/3 of the scale on the first range.

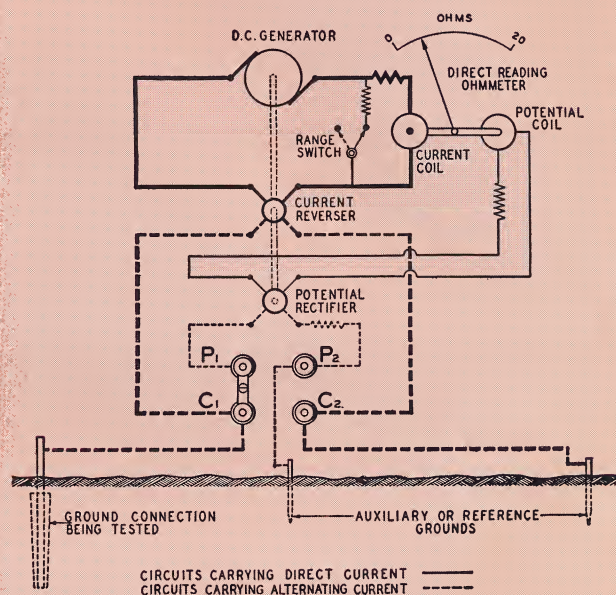


FIGURE 4—Simplified diagram showing the principle of operation of Megger Earth Tester, Catalog 601.

MEGGER® NULL BALANCE EARTH TESTER

A new highly sensitive method of measuring earth resistance

Designed to meet hard field service with fine laboratory performance

FEATURES

Range: 0.01 ohm to 9990 ohms in four overlapping ranges.

Accuracy: $\pm 1\%$ of range in use even on the lowest range with probe resistances up to 1500 ohms.

Guard Terminal: Used to assure accuracy when extremely high probe resistances are encountered. Variable a-c output eliminates effects of stray currents and soil electrolysis.

Digital read-out "at a glance"—remains in view until re-switched.

Strong metal case particularly suited for field use—fitted with sling type carrying strap—weight of this self-contained instrument only 9 pounds.

The accuracy of this instrument is not affected by electrode resistance.

To obtain high accuracy, proper internal guarding is necessary to prevent leakage currents from being introduced into the system. The guard wiring is connected to the Guard Terminal for use when the probe resistances are high or unbalanced.

The test current, obtained from a hand cranked a-c generator, is passed to the ground under test and returned through the soil to the C_2 terminal. The test current also passes through the primary of a current transformer. The secondary of the current transformer generates a potential which is applied in opposition to the potential generated by the test current developed between the potential terminals P_1 and P_2 . By means of an adjustable measuring resistance the potential generated in the secondary of the current transformer



FIGURE 5—Megger Earth Tester 63220

is balanced against the test potential between terminals P_1 and P_2 . The adjustable potentiometer is calibrated directly in terms of earth resistance, ohms. When the zero center galvanometer is at balance the earth rod resistance, etc., is read instantly by the digital read-out.

The instrument will measure resistance from 0.01 to 9990 ohms in four ranges. The readings are given by means of three separate digital indicators. An extremely high degree of accuracy is obtained even on the lower range, with individual spike resistances up to 1500 ohms. On higher ranges, much greater spike resistances than this can be tolerated without affecting performance. Applications include:

Earth electrode resistance measurement

Soil Resistivity measurement

Earth Continuity testing

Neutral Earth Test

Direct resistance measurement within the instrument range

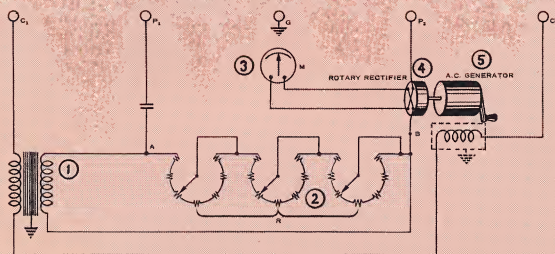


FIGURE 6—Simplified circuit diagram of Megger Earth Tester

- | | |
|---------------------|-------------------------|
| 1. Transformer | 4. Mechanical Rectifier |
| 2. Digital Switches | 5. A-C Generator |
| 3. Galvanometer | |

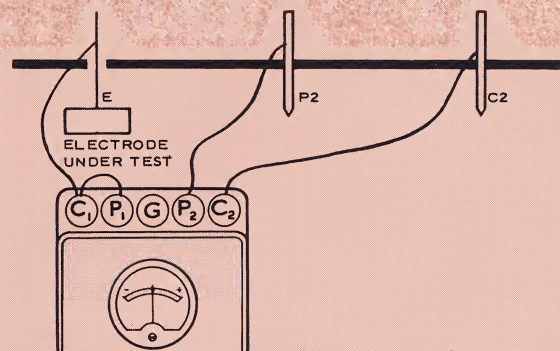


FIGURE 7—Typical Test Connections



FIGURE 8—8742 leather carrying case for Megger Earth Tester 601.



FIGURE 9—665 wood traveling case with cushion packing for Megger Earth Tester 601, suitable for shipment.

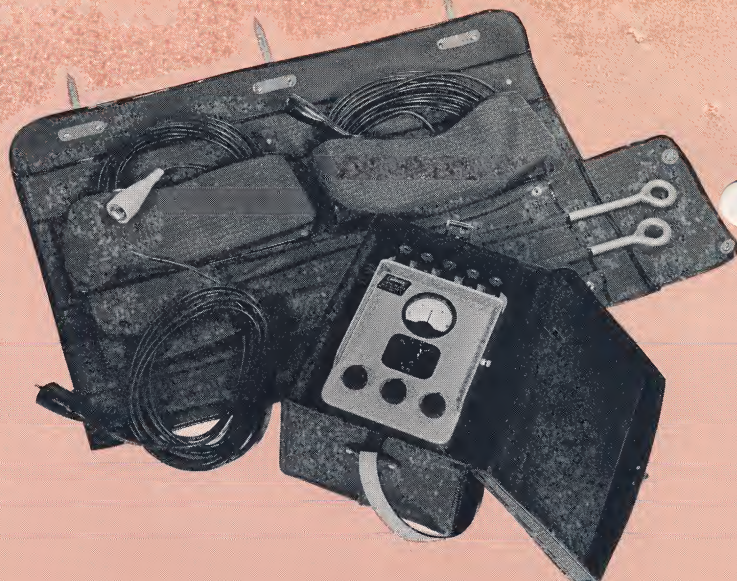


FIGURE 10—Megger Null Balance Earth Tester in leather case 63850 with kit 63579 of rods and leads.

ORDERING INFORMATION

CATALOG NO.	DESCRIPTION	SHIPPING WEIGHT	
		NET	GROSS
601	Megger Heavy-Duty, Multi-Range Earth Tester with Ranges 0 to 20, 0 to 200, 0 to 2000 and 0 to 20,000 ohms	22 lbs.	35 lbs.
63220	Megger Null Balance Earth Tester with range of 0.01 ohm to 9990 ohms in four overlapping ranges.	9 lbs.	14 lbs.
ACCESSORIES—CARRYING CASES			
665	Wood Case with cushion packing for 601	14 lbs.	20 lbs.
8742	Leather Case for 601	5 lbs.	7 lbs.
63850	Leather Case for 63220	4 lbs.	6 lbs.
ACCESSORIES—FOR EITHER INSTRUMENT			
63576	Set of 3 leads; 1-25', 1-50' and 1-100'	8 lbs.	10 lbs.
63578	Heavy Canvas Carry-all; will hold 576 leads and two pairs of rods 580 or 582	2 lbs.	5 lbs.
63580	Pair of 20" Ground Rods with hardened points and loop for easy removal	3 lbs.	5 lbs.
63582	Pair of 30" heavy-duty ground rods with hardened points and loop for easy removal. For difficult terrain such as hard rocky soils	6 lbs.	9 lbs.
942	Test Record Cards (5" x 8"—Universal)	1¼ lb. per C.	
63579	Accessory Kit consisting of 578 Carry-all, 576 Leads and 580 Ground Rods	13 lbs.	18 lbs.



Tells You How to Use

MEGGER® EARTH TESTERS

This 48-page book entitled "Getting Down-to-Earth" covers the important subject of earth testing in a way that practical electrical men appreciate. It provides a detailed explanation of the importance of measuring earth resistance for electrical grounding systems. It goes into the subject of earth resistivity and tells you how to improve grounding systems.

Write for BULLETIN 25T

JAMES G. BIDDLE CO.

Electrical Testing and Speed Measuring Instruments

PLYMOUTH MEETING, PA. 19462 • Area Code 215/Mitchell 6-9200

Printed in U.S.A.

File 4110 50 7-66 W

JAMES G. BIDDLE CO.

Electrical and Speed Measuring Instruments
PLYMOUTH MEETING, PENNSYLVANIA 19462

MEGGER EARTH TESTER

Catalog No.		Price
601	Megger Universal Earth Tester (Instrument Only)	\$750.00
63220	Megger Null Balance Earth Tester (Instrument Only)	290.00
665	Wood Case (for Cat. 601)	65.00
8742	Leather Case (for Cat. 601)	100.00
63850	Leather Case (for Cat. 63220)	40.00
63579	Accessory Kit, consisting of Cat. Nos. 63578, 63576 and 63580 (Formerly Nos. 578, 576 and 580)	80.00
63576	Test Leads, set (one each 25, 50, 100 feet).....	45.00
63578	Canvas Carryall	24.00
63580	Ground Rods - 20" long - pair.....	11.00
63582	Ground Rods - 30" long - pair.....	21.00
942	Test Record Cards	2.50/C

All prices are Net f.o.b. Plymouth Meeting, Pa. Terms: 30 days net

SUBJECT TO CHANGE WITHOUT NOTICE

Minimum Order: \$5.00